

# Reflection and Transmission Characteristics of Coupled Wave through Micropolar Elastic Solid Interlayer in Micropolar Fluid

Xu Hongyu<sup>\*1</sup>, Dang Songyang<sup>2</sup>, Sun Qingyong<sup>3</sup>, Liang Bin<sup>4</sup>

Schematizing and Architectural Engineering School, Henan University of Science and Technology, No.263, Kaiyuan Road, Luoyang, China

<sup>\*</sup>xuhongyu@haust.edu.cn; <sup>2</sup>790952752@qq.com; <sup>3</sup>sun-qing-yong-wo@163.com; <sup>4</sup>liangbin4231@163.com

## Abstract

Based on micropolar fluid theory and micropolar solid elasticity theory, reflection and transmission characteristics of three kinds of micropolar elastic waves involving longitudinal displacement wave and two coupled waves, are studied when incident coupled wave propagates through micropolar elastic solid plate in micropolar fluid. Theoretical and numerical analytical results reveal that in general the amplitude ratios of various reflected and transmitted waves are functions of angle of incidence, frequency of the incident wave and of the material properties of the medium through which they travel. At normal incidence, the reflection and transmission of only coupled wave takes place and no other wave is found to reflect or transmit. At grazing incidence, no reflection or transmission phenomena take place and the same wave propagates along the interface. The rules of the reflection waves and refraction waves amplitudes varied with incident angle are also discussed.

## Keywords

*Micropolar Theory; Reflection; Transmission; Amplitude Ratios; Micropolar Elastic Wave*

## Introduction

Under continuum hypothesis of an elastic body, the classical theory of elasticity is based on linear stress-strain law (Hooke's law). In this theory, the transmission of load across a surface element of an elastic body is described by a force stress and the motion is characterized by translational degrees of freedom only. For materials possessing granular structure, it is found that the classical theory of elasticity is inadequate to represent the complete deformation. Certain discrepancies are observed between the results obtained experimentally and theoretically, particularly, in dynamical problems of waves and vibrations involving high frequencies. Cosserat and Cosserat (1909) was the first who gave importance to the microstructure of a granular body and incorporated a local rotation of points, in addition

to the translation assumed in classical theory of elasticity. This theory is known as 'Cosserat theory' after their names. Mindlin (1964) presented a linear theory of a three-dimensional continuum having the properties of a crystal lattice, including the idea of unit cell. Later, Eringen incorporated micro-inertia and renamed the 'Cosserat elasticity' as the 'Micropolar elasticity'. The linear theory of micropolar elasticity developed by Eringen (1966) is basically an extension of the classical theory of elasticity. With rapid advance of the science and technology, the research in the space of the sandwich structure with the spread of the wave based on micropolar fluid theory has got more and more attention by scholars. The research of wave-absorbing materials is the most significant. Because the stealth and electromagnetic compatibility (EMC) technology become more and more important, the effect of electromagnetic wave absorption material is very outstanding. It becomes a modern military in the magic weapon of the electronic counter and a "secret weapon".

In recent decades, many problems of reflection and refraction of micropolar elastic waves at a plane interface have been studied by several researchers<sup>[1-10]</sup>.

In this paper, based on micropolar fluid theory and micropolar solid elasticity theory, reflection and transmission characteristics of three kinds of micropolar elastic waves involving longitudinal displacement wave and two coupled waves are studied when incident coupled wave propagates through micropolar elastic solid plate in micropolar fluid. The change rules of the reflection waves and refraction waves amplitudes varied with incident angle are also discussed.

## Equations of Motion and Constitutive Relations

In the absence of body force density and body couple

density, for micropolar fluid medium and micropolar solid medium, the equations of motion are given as Eqs.(1) and (2), respectively.

$$\left. \begin{aligned} (c_{1f}^2 + c_{3f}^2) \nabla (\nabla \cdot \mathbf{u}^f) - (c_{2f}^2 + c_{3f}^2) \nabla \times (\nabla \times \mathbf{u}^f) \\ + c_{3f}^2 \nabla \times \dot{\Phi}^f = \ddot{\mathbf{u}}^f \\ (c_{4f}^2 + c_{5f}^2) \nabla (\nabla \cdot \dot{\Phi}^f) - c_{5f}^2 \nabla \times (\nabla \times \dot{\Phi}^f) \\ + c_{6f}^2 (\nabla \times \mathbf{u}^f - 2\dot{\Phi}^f) = \ddot{\Phi}^f \end{aligned} \right\} \quad (1)$$

$$\left. \begin{aligned} (c_{1s}^2 + c_{3s}^2) \nabla (\nabla \cdot \mathbf{u}^s) - (c_{2s}^2 + c_{3s}^2) \nabla \times (\nabla \times \mathbf{u}^s) \\ + c_{3s}^2 \nabla \times \dot{\Phi}^s = \ddot{\mathbf{u}}^s \\ (c_{4s}^2 + c_{5s}^2) \nabla (\nabla \cdot \dot{\Phi}^s) - c_{5s}^2 \nabla \times (\nabla \times \dot{\Phi}^s) \\ + c_{6s}^2 (\nabla \times \mathbf{u}^s - 2\dot{\Phi}^s) = \ddot{\Phi}^s \end{aligned} \right\} \quad (2)$$

where  $c_{1r}^2 = (\lambda^r + 2\mu^r)/\rho^r$ ,  $c_{2r}^2 = \mu^r/\rho^r$ ,  $c_{3r}^2 = K^r/\rho^r$ ,  $c_{4r}^2 = (\alpha^r + \beta^r)/\rho^r j^r$ ,  $c_{5r}^2 = \gamma^r/\rho^r j^r$ ,  $c_{6r}^2 = c_{3r}^2/j^r$ ,  $\rho^r$  is the density of the medium,  $j^r$  is the micro-inertia and  $\mathbf{u}^r$  and  $\Phi^r$  are, respectively, the displacement and microrotation vectors for the micropolar elastic half-spaces. Here, the quantity having superscript  $r$  corresponds to the fluid and solid medium when  $r = f$  and  $r = s$ , respectively.  $\lambda^f$ ,  $\mu^f$  and  $K^f$  are the fluid viscosity coefficients and  $\alpha^f$ ,  $\beta^f$  and  $\gamma^f$  are the fluid viscosity coefficients responsible for gyrational dissipation of the micropolar fluid,  $\lambda^s$ ,  $\mu^s$  are Lamé's constant and  $K^s$ ,  $\alpha^s$ ,  $\beta^s$  and  $\gamma^s$  are the micropolar elastic constants for the micropolar elastic solid.

For micropolar fluid medium and micropolar solid medium, the constitutive relations are given by Eqs.(3) and (4), respectively.

$$\left. \begin{aligned} \tau_{kl}^f = \lambda^f \dot{u}_{r,r}^f \delta_{kl} + \mu^f (\dot{u}_{k,l}^f + \dot{u}_{l,k}^f) + K^f (\dot{u}_{l,k}^f - \varepsilon_{klp} \dot{\phi}_p^f) \\ m_{kl}^f = \alpha^f \dot{\phi}_{r,r}^f \delta_{kl} + \beta^f \dot{\phi}_{k,l}^f + \gamma^f \dot{\phi}_{l,k}^f \end{aligned} \right\} \quad (3)$$

$$\left. \begin{aligned} \tau_{kl}^s = \lambda^s u_{r,r}^s \delta_{kl} + \mu^s (u_{k,l}^s + u_{l,k}^s) + K^s (u_{l,k}^s - \varepsilon_{klp} \phi_p^s) \\ m_{kl}^s = \alpha^s \phi_{r,r}^s \delta_{kl} + \beta^s \phi_{k,l}^s + \gamma^s \phi_{l,k}^s \end{aligned} \right\} \quad (4)$$

where  $\tau_{kl}^r$  is the force stress tensor,  $m_{kl}^r$  is the couple stress tensor, the 'comma' in the subscript denotes the spatial derivative,  $\delta_{kl}$  and  $\varepsilon_{klp}$  are Kronecker delta and the alternating tensors respectively. Other symbols have their usual meanings.

Using Helmholtz theorem, we can write

$$\begin{bmatrix} \mathbf{u}^r \\ \Phi^r \end{bmatrix} = \nabla \begin{bmatrix} A^r \\ C^r \end{bmatrix} + \nabla \times \begin{bmatrix} \mathbf{B}^r \\ \mathbf{D}^r \end{bmatrix}, \quad \nabla \cdot \begin{bmatrix} \mathbf{B}^r \\ \mathbf{D}^r \end{bmatrix} = 0 \quad (5)$$

where  $A^r$  and  $C^r$  are the scalar potentials, while

$\mathbf{B}^r$  and  $\mathbf{D}^r$  are the vector potentials. Plugging Eqs.(5) into Eqs.(1), we can obtain

$$\Pi_1 A^f = 0, \quad \Pi_2 C^f = 0 \quad (6)$$

$$\left. \begin{aligned} (c_{2f}^2 + c_{3f}^2) \nabla^2 \dot{\mathbf{B}}^f + c_{3f}^2 \nabla \times \dot{\mathbf{D}}^f = \ddot{\mathbf{B}}^f \\ c_{5f}^2 \nabla^2 \dot{\mathbf{D}}^f + c_{6f}^2 \nabla \times \dot{\mathbf{B}}^f - 2c_{6f}^2 \dot{\mathbf{D}}^f = \ddot{\mathbf{D}}^f \end{aligned} \right\} \quad (7)$$

where

$$\Pi_1 = \left[ (c_{1f}^2 + c_{3f}^2) \nabla^2 - \frac{\partial}{\partial t} \right] \frac{\partial}{\partial t}$$

$$\text{and } \Pi_2 = \left[ (c_{4f}^2 + c_{5f}^2) \nabla^2 - 2c_{6f}^2 - \frac{\partial}{\partial t} \right] \frac{\partial}{\partial t}.$$

It can be seen that equations in Eqs.(6) are un-coupled in scalar potentials  $A^r$  and  $C^r$  while Eqs. (7) are coupled in vector potentials  $\mathbf{B}^r$  and  $\mathbf{D}^r$ .

### Plane Wave of Micropolar Fluid and Solid

Take the form of a plane wave propagating in the positive direction of a unit vector  $\mathbf{n}$  as

$$\{A^r, C^r, \mathbf{B}^r, \mathbf{D}^r\} = \{a^r, c^r, \mathbf{b}^r, \mathbf{d}^r\} \exp\{ik(\mathbf{n} \cdot \mathbf{r} - Vt)\} \quad (8)$$

where  $a^r, c^r, \mathbf{b}^r$  and  $\mathbf{d}^r$  are constants,  $\mathbf{r} (= x\bar{i} + y\bar{j} + z\bar{k})$

is the position vector,  $V$  is the phase velocity in the direction of  $\mathbf{n}$ ,  $k (= \omega/V)$  is the wave number,  $\omega$  is the angular frequency.

Parfitt and Eringen (1969) have already shown that there exist four waves in an infinite micropolar elastic solid medium propagating with distinct phase velocities. The four phase velocities are given as follows.

(i) an independent longitudinal displacement wave propagating with phase velocity  $V_{s1} = c_{1s}^2 + c_{3s}^2$

(ii) two sets of coupled waves, each consists of a transverse displacement wave and a transverse microrotational wave perpendicular to it, propagating with phase velocities  $V_{s2}$  and  $V_{s3}$  given by  $V_{s2,s3}^2 = (b \pm \sqrt{b^2 - 4ac})/2a$ , where

$$\omega_0^2 = c_{6s}^2, \quad a = 1 - 2\omega_0^2/\omega^2,$$

$$b = c_{2s}^2 + c_{3s}^2 + c_{5s}^2 - (2c_{2s}^2 + c_{3s}^2)\omega_0^2/\omega^2, \quad c = c_{5s}^2(c_{2s}^2 + c_{3s}^2)$$

(iii) an independent longitudinal microrotational wave propagating with phase velocity  $V_{s4}^2 = (c_{4s}^2 + c_{5s}^2)(1 - 2\omega_0^2/\omega^2)^{-1}$ .

Similarly, Singh and Tomar have given that there exist four waves in an infinite micropolar fluid medium propagating with distinct phase velocities.

The four phase velocities are given by

$$V_{f1}^2 = -i\omega(c_{1f}^2 + c_{3f}^2), V_{f2,f3}^2 = (-b' \pm \sqrt{b'^2 - 4a'c'}) / 2a',$$

$$V_{f4}^2 = -i\omega^2(c_{4f}^2 + c_{5f}^2)(\omega + 2ic_{6f}^2)^{-1},$$

where

$$a' = \omega + 2ic_{6f}^2,$$

$$b' = \omega[i\omega c_{5f}^2 + i(c_{2f}^2 + c_{3f}^2)(\omega + 2ic_{6f}^2) + c_{3f}^2 c_{6f}^2]$$

$$\text{and } c' = -\omega^3 c_{5f}^2 (c_{2f}^2 + c_{3f}^2).$$

### Reflection and Transmission of Coupled Wave

Introducing the Cartesian coordinates  $x$ ,  $y$  and  $z$  such that  $xy$  plane ( $z=0$ ) is interface. Thickness of  $d$  micropolar solid placed between micropolar fluid, the  $z$ -axis is taken perpendicular to the interface ( $z=0$ ) and pointing downward into the medium  $M_2$ . We shall consider a two-dimensional problem in  $xz$  plane, so that the followings are the displacement and microrotational vectors in micropolar elastic solid and in micropolar fluid:

$$\mathbf{u}^r = (u_1^r(x, z), 0, u_3^r(x, z)), \quad \Phi^r = (0, \Phi_2^r, 0) \quad (r=f, s) \quad (9)$$

The plan couple wave incident to interface  $z=0$  with phase velocity  $V_{f1}$  and incident angle  $\theta_0$  within micropolar fluid propagation and then entrance to micropolar solid medium  $M_2$  and incident into interface  $z=d$  go through medium  $M_2$ , then entrance to micropolar fluid medium  $M_1$ .

We take the following form of potentials:

Interface  $z=0$ : when  $z \leq 0$ , in micropolar fluid medium  $M_1$ ,

$$\{A^f, B_2^f, \phi_2^f\}^T = \left\{ \begin{array}{l} A_0 \exp(\chi_0) + A_1' \exp(\chi_1') \\ \sum_{i=2}^3 A_i' \exp(\chi_i') \\ \sum_{i=2}^3 \eta_i' A_i' \exp(\chi_i') \end{array} \right\} \quad (10)$$

And when  $0 \leq z \leq d$ , in micropolar solid medium  $M_2$

$$\{A^s, B_2^s, \phi_2^s\}^T = \left\{ \begin{array}{l} A_1 \exp(\chi_1) \\ \sum_{i=2}^3 A_i \exp(\chi_i) \\ \sum_{i=2}^3 \eta_i A_i \exp(\chi_i) \end{array} \right\} \quad (11)$$

where  $A_0$ ,  $A_1$  and  $A_1'$  are the amplitude of the incident, reflected and refracted longitudinal displacement wave, respectively.  $A_2$ ,  $A_3$  and  $A_2'$ ,  $A_3'$  are the amplitude of the reflected and refracted couple wave.

$$\chi_0 = ik_1'(\sin \theta_0 x + \cos \theta_0 z) - i\omega_1' t,$$

$$\chi_i = ik_i(\sin \theta_i x + \cos \theta_i z) - i\omega_i t,$$

$$\chi_i' = ik_i'(\sin \theta_i' x - \cos \theta_i' z) - i\omega_i' t, \quad (i=1, 2, 3).$$

When  $d \leq z$ , in micropolar fluid medium  $M_1$ , for longitudinal displacement wave:

$$\left\{ \begin{array}{l} \{A^s, B_2^s, \phi_2^s\} = \left\{ \begin{array}{l} A_1 \exp(\chi_1) + B_1 \exp(\chi_1^0), \\ \sum_{i=2}^3 B_i \exp(\chi_i^0), \sum_{i=2}^3 \eta_i B_i \exp(\chi_i^0) \end{array} \right\} \\ \{A^f, B_2^f, \phi_2^f\} = \left\{ \begin{array}{l} B_1' \exp(\chi_1''), \sum_{i=2}^3 B_i' \exp(\chi_i''), \\ \sum_{i=2}^3 \eta_i' B_i' \exp(\chi_i'') \end{array} \right\} \end{array} \right\} \quad (12)$$

For couple wave I, ( $j=2, 3$ )

$$\left\{ \begin{array}{l} \{A^s, B_2^s, \phi_2^s\}^T = \left\{ \begin{array}{l} B_4 \exp(\chi_4^0) \\ A_2 \exp(\chi_2) + \sum_{i=5}^6 B_i \exp(\chi_i^0) \\ \sum_{i=5}^6 \eta_j B_i \exp(\chi_i^0) \end{array} \right\} \\ \{A^f, B_2^f, \phi_2^f\}^T = \left\{ \begin{array}{l} B_4' \exp(\chi_4'') \\ \sum_{i=5}^6 B_i' \exp(\chi_i'') \\ \sum_{i=5}^6 \eta_j' B_i' \exp(\chi_i'') \end{array} \right\} \end{array} \right\} \quad (13)$$

For couple wave II, ( $j=2, 3$ )

$$\left\{ \begin{array}{l} \{A^s, B_2^s, \phi_2^s\}^T = \left\{ \begin{array}{l} B_7 \exp(\chi_7^0) \\ \sum_{i=8}^9 B_i \exp(\chi_i^0) \\ A_3 \exp(\chi_3) + \sum_{i=8}^9 \eta_j B_i \exp(\chi_i^0) \end{array} \right\} \\ \{A^f, B_2^f, \phi_2^f\}^T = \left\{ \begin{array}{l} B_7' \exp(\chi_7'') \\ \sum_{i=8}^9 B_i' \exp(\chi_i'') \\ \sum_{i=8}^9 \eta_j' B_i' \exp(\chi_i'') \end{array} \right\} \end{array} \right\} \quad (14)$$

where  $B_i$  and  $B_i'$  are the amplitude of reflected and refracted longitudinal displacement wave or coupled wave, respectively.

$$\chi_i^0 = ik_i(\sin \varphi_i x - \cos \varphi_i z) - i\omega_i^0 t,$$

$\chi_i'' = ik_i'(\sin \varphi_i'' x + \cos \varphi_i'' z) - i\omega_i'' t$ , ( $i=1, 2, \dots, 9$ ). The coupling parameters  $\eta_{2,3}$  and  $\eta_{2,3}'$  are given by:

$$\eta_{2,3} = -c_{6s}^2 \left[ V_{s2,s3}^2 - 2 \frac{c_{6s}^2}{k_{2,3}^2} - c_{5s}^2 \right]^{-1},$$

$$\eta'_{2,3} = ic_{6f}^2 \left[ \frac{V_{f2,f3}}{k'_{2,3}} + 2 \frac{ic_{6f}^2}{k_{2,3}^2} + ic_{5f}^2 \right]^{-1}.$$

Boundary conditions to be satisfied at the interface  $z=0$  and  $z=d$ , are the continuity of force stress, couple stress, displacement and microrotation. Mathematically, these boundary conditions can be written as:

$$\tau_{zz}^s = \tau_{zz}^f, \tau_{zy}^s = \tau_{zy}^f, m_{zy}^s = m_{zy}^f, u_1^s = u_1^f, u_3^s = u_3^f, \phi_2^s = \phi_2^f \quad (15)$$

Employing the Snell's law given by:

$$\frac{\sin \theta_0}{V_{fi}} = \frac{\sin \theta_i}{V_{si}} = \frac{\sin \theta'_i}{V_{fi}} = \frac{\sin \phi_i}{V_{si}} = \frac{\sin \phi_{i+3}}{V_{si}} = \frac{\sin \phi_{i+6}}{V_{si}}$$

$$= \frac{\sin \phi'_i}{V_{fi}} = \frac{\sin \phi'_{i+3}}{V_{fi}} = \frac{\sin \phi'_{i+6}}{V_{fi}}, \quad (i=1,2,3)$$

and assuming that all frequencies are equal at the interface, 24 homogeneous equations can be obtained and can be written in a matrix form as:

$$\mathbf{PZ} = \mathbf{Q} \quad (16)$$

where

$$\mathbf{P} = [a_{ij}]_{24 \times 24}, \mathbf{Z} = [z_k]^T \quad (k=1,2,\dots,24),$$

$$\mathbf{Q} = [110110000000000000000000]^T.$$

The entries of the matrix  $\mathbf{P}$  and the elements of the matrix  $\mathbf{Z}$  are given in Appendix.

## Numerical Results and Discussions

The paper presents numerical example to explore the transmission characteristics of incident longitudinal displacement wave when throughing the micropolar fluids of micropolar elastic plate. For numerical computations, we take the values of the relevant parameters from Hsia(2006)[9].

For micropolar viscous fluid  $M_1$ :

$$\lambda^f = 1.5 \times 10^{10} \text{ dyne s/cm}^2,$$

$$\mu^f = 0.3 \times 10^{10} \text{ dyne s/cm}^2,$$

$$K^f = 0.00223 \times 10^{10} \text{ dyne s/cm}^2,$$

$$\alpha^f = 0.00111 \times 10^{10} \text{ dyne s},$$

$$\beta^f = 0.0022 \times 10^{10} \text{ dyne s},$$

$$\gamma^f = 0.000222 \times 10^{10} \text{ dyne s},$$

$$j^f = 0.0400 \text{ cm}^2,$$

$$\rho^f = 0.8 \text{ g/cm}^3.$$

For micropolar elastic solid  $M_2$ :

$$\lambda^s = 2.09730 \times 10^{10} \text{ dyne/cm}^2,$$

$$\mu^s = 0.91822 \times 10^{10} \text{ dyne/cm}^2,$$

$$K^s = 0.22965 \times 10^{10} \text{ dyne/cm}^2,$$

$$\alpha^s = -0.0000291 \times 10^{10} \text{ dyne},$$

$$\beta^s = 0.000045 \times 10^{10} \text{ dyne},$$

$$\gamma^s = 0.0000423 \times 10^{10} \text{ dyne},$$

$$j^s = 0.037 \text{ cm}^2,$$

$$\rho^s = 0.0034 \text{ g/cm}^3.$$

And  $\omega/\omega_0 = 100$  and thickness of the interlayer:  $d=0.01\text{m}$ . The system of equations given by Eqs.(16) are solved by Gauss elimination method. The values of the amplitude ratios are computed at different angles of incidence.

From FIG.1 to FIG.6, we get the curve of three kinds of wave reflection and transmission coefficient with the angle of incidence changed after coupled wave through micropolar elastic solid plate in micropolar fluid.

FIG.1 shows that the variation of the amplitude ratios of reflected longitudinal displacement waves with the incidence angle  $\theta_0$ , when a plane coupled wave propagates from the micropolar fluid half-space with phase velocity  $V_{f2}$ . The amplitude ratio of longitudinal displacement wave has two peak value when incidence angle  $\theta_0$  is  $27.7^\circ$  or  $68.6^\circ$ , respectively. And it is zero when  $\theta_0 = 45^\circ$ .

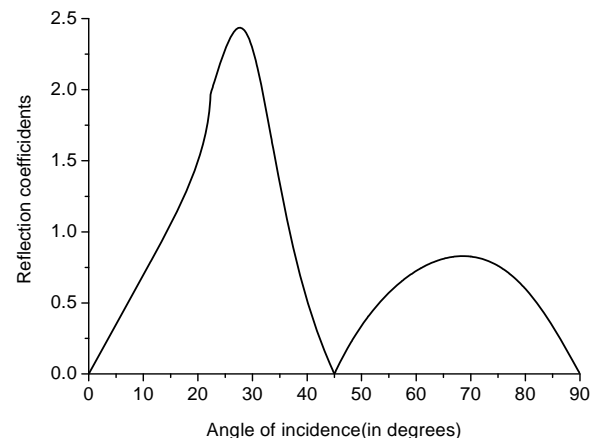


FIG. 1 REFLECTION COEFFICIENT OF LONGITUDINAL DISPLACEMENT WAVE

FIG.2 shows that the variation of the amplitude ratios of reflected coupled wave I with the incidence angle  $\theta_0$ . The amplitude ratio of coupled wave I has the minimal value when  $\theta_0$  is  $19.1^\circ$ . It decreases monotonically from the value 1.0 to the value 0.7784 at

$\theta_0 = 19.1^\circ$  and then it increases rapidly. The amplitude ratio of coupled wave II gets to the maximum value when  $\theta_0$  is about  $23^\circ$ . And then, the change of incidence angle has no effect on the amplitude ratio of coupled waves.

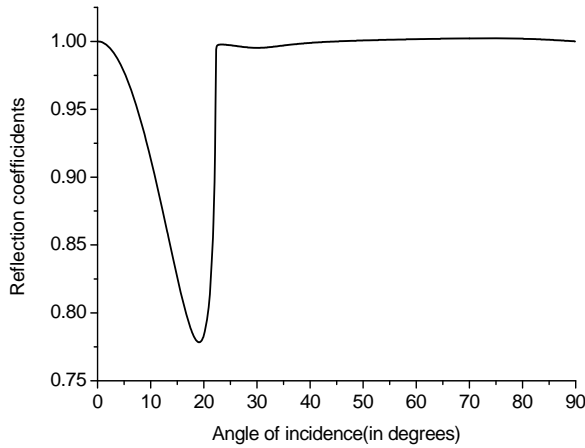


FIG. 2 REFLECTION COEFFICIENT OF COUPLE WAVE I

FIG.3 shows that the variation of the amplitude ratios of reflected coupled wave II with the incidence angle  $\theta_0$ . The variation of the amplitude ratio of coupled wave II decreases slowly at first. It reaches the minimal value when  $\theta_0$  is about  $20^\circ$ . It suddenly rears up at about  $23^\circ$  in the range of  $5^\circ$ . It declines sharply to zero when  $\theta_0$  is about  $45^\circ$ . And then it gradually increases to the peak value at about  $73^\circ$ . At last, it decreases to zero gradually.

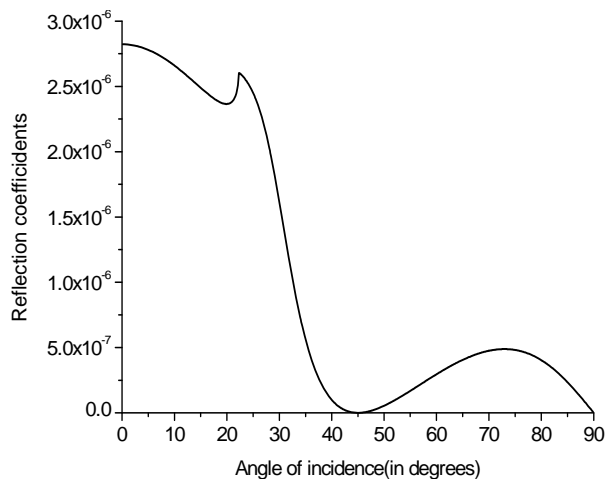


FIG. 3 REFLECTION COEFFICIENT OF COUPLE WAVE II

FIG.4 shows that the variation of the amplitude ratio of transmission longitudinal displacement wave with the incidence angle  $\theta_0$ , when a plane coupled wave propagates from the micropolar fluid half-space with phase velocity  $V_{t2}$ . The amplitude ratio of longitudinal displacement wave has two peak value when

incidence angle  $\theta_0$  is  $28.3^\circ$  or  $73^\circ$ , respectively. The curve fluctuates at  $23^\circ$ . The amplitude ratio of of transmission longitudinal displacement wave is zero when  $\theta_0$  is about  $45^\circ$ .

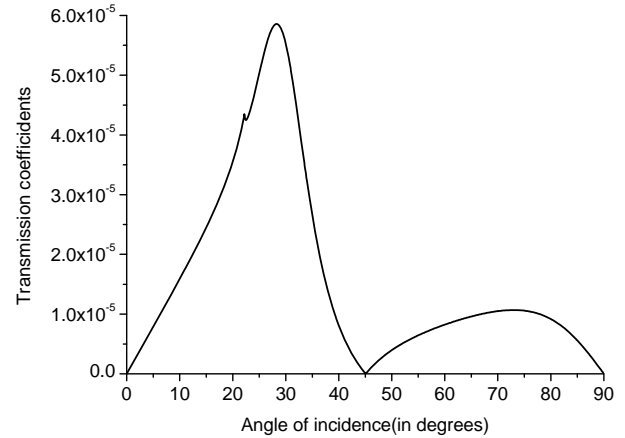


FIG. 4 TRANSMISSION COEFFICIENT OF LONGITUDINAL DISPLACEMENT WAVE

FIG.5 shows that the variation of the amplitude ratio of transmission couple wave I with the incidence angle  $\theta_0$ . The variation of the amplitude ratio of coupled wave I changed slowly at first. Then it reaches to the peak value when  $\theta_0$  is about  $30^\circ$ . It declines sharply in the range of  $10^\circ$ . And then, the curve changes gently at about  $67^\circ$ . At last it decreases gradually to zero when  $\theta_0$  is  $90^\circ$ .

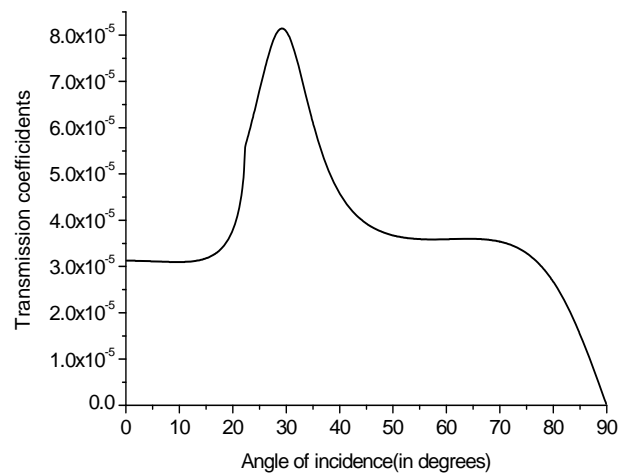


FIG. 5 TRANSMISSION COEFFICIENT OF COUPLE WAVE I

FIG.6 shows that the variation of the amplitude ratio of transmission couple wave II with the incidence angle  $\theta_0$ . The shape of the curve likes the transmission couple wave I, but the amplitude ratio of couple wave II is small than that of couple wave I about four orders of magnitude.

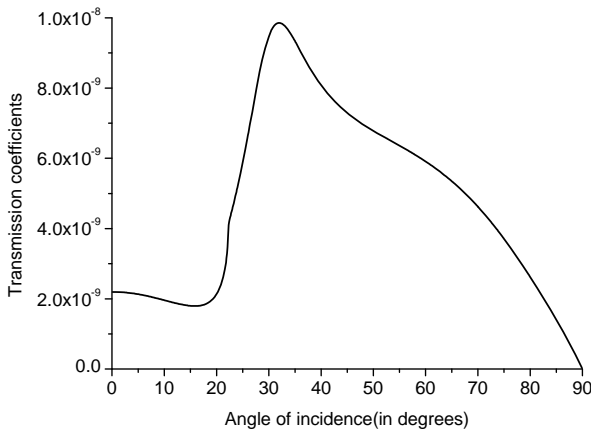


FIG. 6 TRANSMISSION COEFFICIENT OF COUPLE WAVE II

From FIG.1 and FIG.6, it can be seen that at normal incidence the reflection and transmission of only reflected couple wave I take place and no other wave is found to reflect or transmit. At grazing incidence no reflection or transmission phenomena take place and the same wave propagates along the interface.

### Conclusions

Based on micropolar fluid theory and micropolar solid elasticity theory, the reflection and transmission phenomena of an coupled wave propagating through the micropolar elastic solid infinite plate in micropolar fluid was discussed. Theoretical and analytical results reveal that, in general, the amplitude ratios of various reflected and transmitted waves are functions of angle of incidence, of frequency of the incident wave and of the material properties of the medium through which they travel. Get three kinds of micropolar elastic wave's curves of reflection coefficient or transmission coefficient with the change of incident angle through the numerical results, and get the varying pattern of reflection and transmission coefficient: there is a maximum value in the curve of reflection coefficient or transmission coefficient of coupled wave, and there are two extremum in the curve of reflection coefficient or transmission coefficient of longitudinal displacement wave.

Based on the specific medium material parameters given by the paper, we conclude that:

(1) At normal incidence, the reflection and transmission of only coupled waves take place and no longitudinal displacement wave is found to reflect or transmit. At grazing incidence, no reflection or transmission phenomena take place and the same wave propagates along the interface.

(2) There exist maximum values of reflection and

transmission coefficient for coupled wave. There exist peak values of reflection and transmission coefficient for longitudinal displacement wave.

(3) There exist zero values of reflection and transmission coefficient for longitudinal displacement wave when incidence angle is  $45^\circ$ , at the same time, transmission coefficient presents wave phenomenon when incidence angle is  $23^\circ$ .

### ACKNOWLEDGMENT

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### Appendix

The component  $a_{ij}$  of the matrix  $\mathbf{P}$  in non-dimensional form are given by

$$\begin{aligned}
 a_{11} &= L_1/L_0, \quad a_{12} = -L_2/L_0, \quad a_{13} = -L_3/L_0, \quad a_{15} = L_4/L_0, \\
 a_{16} &= L_5/L_0, \quad a_{21} = M_1/M_0, \quad a_{22} = M_4/M_0, \quad a_{23} = M_5/M_0, \\
 a_{25} &= -M_6/M_0, \quad a_{26} = -M_7/M_0, \quad a_{32} = -N_2, \quad a_{33} = -N_3, \\
 a_{35} &= -N_4, \quad a_{36} = -N_5, \quad a_{41} = P_1/P_0, \quad a_{42} = -P_2/P_0, \\
 a_{43} &= -P_3/P_0, \quad a_{45} = P_4/P_0, \quad a_{46} = P_5/P_0, \quad a_{51} = Q_1/Q_0, \\
 a_{52} &= Q_2/Q_0, \quad a_{53} = Q_3/Q_0, \quad a_{55} = -Q_4/Q_0, \quad a_{56} = -Q_5/Q_0, \\
 a_{62} &= \eta_2, \quad a_{63} = \eta_3, \quad a_{65} = -\eta'_2, \quad a_{66} = -\eta'_3, \quad a_{71} = L_1\xi_1^{-1}, \\
 a_{77} &= L_1\xi_1, \quad a_{78} = L_2\xi_2, \quad a_{79} = L_3\xi_3, \quad a_{710} = -L_0\xi'_1, \quad a_{711} = -L_4\xi'_2, \\
 a_{712} &= -L_5\xi'_3, \quad a_{81} = M_1\xi_1^{-1}, \quad a_{87} = -M_1\xi'_1, \quad a_{88} = M_4\xi_2, \\
 a_{89} &= M_5\xi_3, \quad a_{810} = -M_0\xi'_1, \quad a_{811} = -M_6\xi'_2, \quad a_{812} = -M_7\xi'_3, \\
 a_{98} &= N_2\xi_2, \quad a_{99} = N_3\xi_3, \quad a_{911} = -N_4\xi'_2, \quad a_{912} = -N_5\xi'_3, \\
 a_{101} &= P_1\xi_1^{-1}, \quad a_{107} = P_1\xi'_1, \quad a_{108} = P_2\xi_2, \quad a_{109} = P_3\xi_3, \\
 a_{1010} &= -P_0\xi'_1, \quad a_{1011} = -P_4\xi'_2, \quad a_{1012} = -P_5\xi'_3, \quad a_{111} = Q_1\xi_1^{-1}, \\
 a_{117} &= -Q_1\xi_1, \quad a_{118} = Q_2\xi_2, \quad a_{119} = Q_3\xi_3, \quad a_{1110} = -Q_0\xi'_1, \\
 a_{1111} &= -Q_4\xi'_2, \quad a_{1112} = -Q_5\xi'_3, \quad a_{128} = \eta_2\xi_2, \quad a_{129} = \eta_3\xi_3, \\
 a_{1211} &= -\eta'_2\xi'_1, \quad a_{1212} = -\eta'_3\xi'_1, \quad a_{1312} = -L_2\xi_2, \quad a_{1313} = L_1\xi_1, \\
 a_{1314} &= L_2\xi_2, \quad a_{1315} = L_3\xi_3, \quad a_{1316} = -L_0\xi'_1, \quad a_{1317} = -L_4\xi'_2, \\
 a_{1318} &= -L_5\xi'_3, \quad a_{142} = M_2\xi_2^{-1}, \quad a_{1413} = -M_1\xi'_1, \quad a_{1414} = M_4\xi_2, \\
 a_{1415} &= M_5\xi_3, \quad a_{1416} = -M_0\xi'_1, \quad a_{1417} = -M_6\xi'_2, \quad a_{1418} = -M_7\xi'_3, \\
 a_{1514} &= N_2\xi_2, \quad a_{1515} = N_3\xi_3, \quad a_{1517} = -N_4\xi'_2, \quad a_{1518} = -N_5\xi'_3, \\
 a_{162} &= -P_2\xi_2^{-1}, \quad a_{1613} = P_1\xi'_1, \quad a_{1614} = P_2\xi_2, \quad a_{1615} = P_3\xi_3, \\
 a_{1616} &= -P_0\xi'_1, \quad a_{1617} = -P_4\xi'_2, \quad a_{1618} = -P_5\xi'_3, \quad a_{172} = Q_2\xi_2^{-1}, \\
 a_{173} &= \eta_3, \quad a_{1713} = -Q_1\xi'_1, \quad a_{1714} = Q_2\xi_2, \quad a_{1715} = Q_3\xi_3, \\
 a_{1716} &= -Q_0\xi'_1, \quad a_{1717} = -Q_4\xi'_2, \quad a_{1718} = -Q_5\xi'_3, \quad a_{1814} = \eta_2\xi_2, \\
 a_{1815} &= \eta_3\xi_3, \quad a_{1817} = -\eta'_2\xi'_1, \quad a_{1818} = -\eta'_3\xi'_1, \quad a_{1919} = L_1\xi_1, \\
 a_{1920} &= L_2\xi_2, \quad a_{1921} = L_3\xi_3, \quad a_{1922} = -L_0\xi'_1, \quad a_{1923} = -L_4\xi'_2, \\
 a_{1924} &= -L_5\xi'_3, \quad a_{203} = M_3\xi_3^{-1}, \quad a_{2019} = -M_1\xi'_1, \quad a_{2020} = M_4\xi_2,
 \end{aligned}$$

$a_{2021} = M_5 \xi_3, a_{2022} = -M_0 \xi_1', a_{2023} = -M_6 \xi_2', a_{2024} = -M_7 \xi_3',$   
 $a_{213} = N_1 \xi_3^{-1}, a_{2120} = N_2 \xi_2, a_{2121} = N_3 \xi_3, a_{2123} = -N_4 \xi_2',$   
 $a_{2124} = -N_5 \xi_3', a_{2219} = P_1 \xi_1, a_{2220} = P_2 \xi_2, a_{2221} = P_3 \xi_3,$   
 $a_{2222} = -P_0 \xi_1', a_{2223} = -P_4 \xi_2', a_{2224} = -P_5 \xi_3', a_{2319} = -Q_1 \xi_1,$   
 $a_{2320} = Q_2 \xi_2, a_{2321} = Q_3 \xi_3, a_{2322} = -Q_0 \xi_1', a_{2323} = -Q_4 \xi_2',$   
 $a_{2324} = -Q_5 \xi_3', a_{243} = \xi_3^{-1}, a_{2420} = \eta_2 \xi_2, a_{2421} = \eta_3 \xi_3,$   
 $a_{2423} = -\eta_2' \xi_2', a_{2424} = -\eta_3' \xi_3', -a_{14} = a_{24} = -a_{44} = a_{54} = 1,$   
 and other items are zero, where

$$L_0 = i\omega k_1'^2 \left[ \lambda^f + (2\mu^f + K^f) \cos^2 \theta_0 \right],$$

$$L_1 = -k_1^2 \left[ \lambda^s + (2\mu^s + K^s) \cos^2 \theta_1 \right],$$

$$L_{2,3} = k_{2,3}^2 (2\mu^s + K^s) \sin \theta_{2,3} \cos \theta_{2,3},$$

$$L_{4,5} = i\omega k_{2,3}'^2 (2\mu^f + K^f) \sin \theta_{2,3}' \cos \theta_{2,3}', M_3 = -K^s,$$

$$M_0 = i\omega k_1'^2 (2\mu^f + K^f) \sin \theta_0 \cos \theta_0,$$

$$M_1 = -k_1^2 (2\mu^s + K^s) \sin \theta_1 \cos \theta_1,$$

$$M_2 = k_2^2 \left[ \mu^s (1 - 2 \sin^2 \theta_2) + K^s \cos^2 \theta_2 \right],$$

$$M_{4,5} = k_{2,3}^2 \left[ \mu^s (1 - 2 \sin^2 \theta_{2,3}) + K^s \cos^2 \theta_{2,3} \right] - K^s \eta_{2,3},$$

$$M_{6,7} = -i\omega k_{2,3}'^2 \left[ \mu^f (1 - 2 \sin^2 \theta_{2,3}') + K^f \cos^2 \theta_{2,3}' \right] - K^f \eta_{2,3}',$$

$$N_1 = i\gamma^s k_3 \cos \theta_3, N_{2,3} = -i\gamma^s \eta_{2,3} k_{2,3} \cos \theta_{2,3},$$

$$N_{4,5} = -\gamma^f \eta_{2,3}' \omega k_{2,3}' \cos \theta_{2,3}', P_0 = ik_1' \sin \theta_0, P_1 = ik_1 \sin \theta_1,$$

$$P_{2,3} = -ik_{2,3} \cos \theta_{2,3}, P_{4,5} = ik_{2,3}' \sin \theta_{2,3}', Q_0 = ik_1' \cos \theta_0,$$

$$Q_{1,2,3} = ik_{1,2,3} \cos \theta_{1,2,3}, Q_{4,5} = ik_{2,3}' \sin \theta_{2,3}',$$

$$\xi_{1,2,3} = \exp(-ik_{1,2,3} \cos \theta_{1,2,3} d),$$

$$\xi_{1,2,3}' = \exp(ik_{1,2,3}' \cos \theta_{1,2,3}' d).$$

The vector  $Z$ :  $Z_i = A_i/A_0$ ,  $Z_{i+3} = A_i'/A_0$ ,  $Z_{i+6} = B_i/A_0$ ,  
 $Z_{i+9} = B_i'/A_0$ ,  $Z_{i+12} = B_{i+3}/A_0$ ,  $Z_{i+15} = B_{i+3}'/A_0$ ,  
 $Z_{i+18} = B_{i+6}/A_0$ ,  $Z_{i+21} = B_{i+6}'/A_0$ . ( $i=1,2,3$ ).

where: when interface  $z=0$ ,  $Z_1$ ,  $Z_2$  and  $Z_3$  are the amplitude ratios for the refracted longitudinal displacement wave or coupled wave, respectively.  $Z_4$ ,  $Z_5$  and  $Z_6$  are the amplitude ratios for the reflected longitudinal displacement wave or coupled wave, respectively; when interface  $z=d$ ,  $Z_7$ ,  $Z_8$ ,  $Z_9$ ,  $Z_{13}$ ,  $Z_{14}$ ,  $Z_{15}$ ,  $Z_{19}$ ,  $Z_{20}$  and  $Z_{21}$  are the amplitude ratios for the reflected longitudinal displacement wave or coupled wave, respectively;  $Z_{10}$ ,  $Z_{11}$ ,  $Z_{12}$ ,  $Z_{16}$ ,  $Z_{17}$ ,  $Z_{18}$ ,  $Z_{22}$ ,  $Z_{23}$  and  $Z_{24}$  are the amplitude ratios for the refracted longitudinal displacement wave or coupled wave, respectively.

## REFERENCES

Tomar S K, Gogna M L. "Reflection and refraction of

longitudinal microrotational wave at an interface between two different micropolar elastic solids in welded contact". Int. J. Eng. Sci 30(1992): 1637-1646. Accessed January 28, 2010. doi:10.1016/0020-7225(92)90132-Z.

Tomar S K, Gogna M L. "Reflection and refraction of longitudinal wave at an interface between two micropolar elastic solids in welded contact". Journal of the Acoustical Society of America 97 (1995): 822-830. Accessed October 1997. doi: 10.1121/1.421017.

Song Y Q, Xu H Y, Zhang Y C. "Reflection and refraction of micropolar magneto-thermovisco-elastic waves at the interface between two micropolar viscoelastic media". International Journal of Thermophysics 27 (2006): 970-993. Accessed May 2006. doi:10.1007/s10765-006-0048-z.

Khurana A, Tomar S K. "Transmission of longitudinal wave at a plane interface between micropolar elastic and chiral solid half-spaces: Incidence from micropolar half-space". Journal of Sound and Vibration 311 (2008): 973-990. Accessed April 8, 2008. doi: 10.1016/j.jsv.2007.09.032.

Tomar S K, Kumar R. "Wave propagation at liquid/micropolar elastic solid interface". International Journal of Sound and Vibration 225 (1999): 858-869. Accessed May 20, 1999. doi: 10.1006/jsvi.1998.2069.

Tomar S K, Kumar R. "Reflection and refraction of longitudinal displacement wave at a liquid micropolar solid interface". International Journal of Engineering Science 33 (1995): 1507-1515. Accessed August 1995. doi: 10.1016/0020-7225(95)00015-P.

Kumar R, Barak M. "Wave propagation in liquid-saturated porous solid with micropolar elastic skeleton at boundary surface". Applied Mathematics and Mechanics (English Edition) 28 (2007): 337-349. Accessed March 2007. doi: 10.1007/s10483-007-0307-Z.

Singh D, Tomar S K. "Longitudinal waves at a micropolar fluid/solid interface". International Journal of Solids and Structures 45 (2008): 225-244. Accessed January 1, 2007. doi: 10.1016/j.ijsolstr.2007.07.015

Hsia S Y, Su C C. "Propagation of longitudinal waves in micro porous slab sandwiched between elastic half-spaces". Japan Journal of Applied physics 47 (2008): 5581-5590. Accessed July 11, 2008. doi: 10.1143/JJAP.47.5581.

Xu Hongyu, Sun Qingyong, Zhang Wei, Liang Bin.

“Reflection and transmission of longitudinal displacement wave through micropolar elastic plate in micropolar fluid”. Chuan Bo Li Xue/Journal of Ship Mechanics,15 (2011): 1065-1074. Accessed September 2011.

Hsia S Y, Cheng J W. “Longitudinal plane wave propagation in elastic-micropolar porous media”. Jpn. J. Appl. Phys 45 (2006): 1743-1748. Accessed March 8,2006.doi: 10.1143/JJAP.45.1743.

**Xu Hongyu**, Male, Born in 1972, Ph. D, Professor; 6/1996, Bachelor, Lanzhou University; 5/2001, Master, Henan University of Science and Technology; 11/2004, Ph. D, Xi'an Jiaotong University. Recent Research Field: Multi-field coupling between magnetic and thermoelectric, Computational

mechanics and engineering applications; Email: xuhongyu@haust.edu.cn.

**Dang Songyang**, Male, Born in 1988, Bachelor; 6/2011, Bachelor, Zhengzhou Institute of Aeronautical Industry Management; Recent Research Field:Computational mechanics and engineering applications; Email:790952752@qq.com.

**Sun Qingyong**, Male, Born in 1984, Master; 6/2009, Bachelor, Henan University of Science and Technology; 6/2012, Master, Henan University of Science and Technology; Recent Research Field: Computational mechanics and engineering applications; Email:sun-qing-yong-wo@163.com.

**Liang Bin**, Male, Born in 1963, Ph. D, Professor; 6/1981, Bachelor, Lanzhou University; 5/1988, Master, Lanzhou University; 6/1992, Ph. D, Lanzhou University; Recent Research Field: Nonlinear analysis and optimization design of engineering structures;Email:liangbin4231@163.com.